

<b>SOUTH COAST AIR QUALITY MANAGEMENT DISTRICT</b>  <b>ENGINEERING AND COMPLIANCE DIVISION</b>  <b>PERMIT APPLICATION EVALUATION AND CALCULATIONS</b>	PAGES 8	PAGE 1
	APPL NO 500899-900	DATE 12-16-09
	PROCESSED BY LLD	CHECKED BY

**OWNER/OPERATOR:**

COID: 15793

RIVERSIDE COUNTY WASTE MANAGEMENT DEPT, LAMB  
14310 FREDERICK STREET  
MORENO VALLEY, CA 92553

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SENIOR CIVIL ENGINEER  
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**EQUIPMENT LOCATION:**

LAMB CANYON SANITARY LANDFILL  
16411 LAMB CANYON RD & HWY 79  
BEAUMONT, CA 92223

**EQUIPMENT DESCRIPTION**

A/N 500899

LANDFILL GAS FLARING SYSTEM CONSISTING OF:

1. LIQUID KNOCKOUT/PARTICULATE REMOVAL VESSEL, JOHN ZINK, WITH DEMISTER.
2. BLOWER, LANDFILL GAS, AEROVENT, 2000 SCFM MAXIMUM FLOW RATE.
3. FLARE NO. 1, JOHN ZINK, 7'-0" DIA. X 30'-0" H., WITH A MULTI JET BURNER, A PROPANE GAS PILOT, ELECTRIC IGNITER, UV FLAME SENSOR, THERMOCOUPLE WITH TEMPERATURE INDICATOR AND RECORDER, AUTOMATIC SHUTDOWN AND ALARM SYSTEM, AUTOMATIC COMBUSTION AIR REGULATING SYSTEM, TEMPERATURE CONTROLLER AND A FLAME ARRESTOR.

(SEE SAMPLE PERMIT)

A/N 500900

TV REVISION (DE MINIMUS SIGNIFICANT)



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### **INTRODUCTION:**

This application was submitted 07-28-09 as a Class I for modification of the existing landfill gas flare by increasing the heat input from 20.7 mmbtu/hr to 54.6 mmbtu/hr and increasing the flow rate of lfg from 760 scfm to 2000 scfm. The flare is currently under a Permit to Construct A/N 391030 as described under Section H of the facility's TV permit (revision 0 issued 9/9/08).

Initial source test was conducted in 2003 by URS.  
A source test was conducted in 2008 by AirX Testing.

### **PROJECT DESCRIPTION:**

Hours of operation are 24 hr/day, 7 days/week.

(see attached John Zink specs dated August 31, 2000)

Equipment is a John Zink flare, rated at 200 - 2000 scfm of 50% CH<sub>4</sub>. Given a lower heating value of 455 btu/scf, the heat rate of the flare ranges from 5.5 mmbtu/hr to 55 mmbtu/hr. The requested increase in flow and heat input will be within the design parameters of the flare.

### **CALCULATIONS:**

PreMod emissions from NSR in A/N 391030

#### **NO<sub>x</sub>:**

NO<sub>x</sub> emission factor of 0.0527 lb/mmbtu is used to keep emissions increase below significance level. 2003 test shows NO<sub>x</sub> 0.032 lb/mmbtu

$$\begin{aligned}
 \text{PostMod NO}_x (\text{max}) &= (0.0527 \text{ lb/mmbtu})(54.6 \text{ mmbtu/hr}) \\
 &= 2.88 \text{ lb/hr} \\
 *24 &= 69.06 \text{ lb/day} \\
 *365 &= 25206.2 \text{ lb/yr} \\
 &= 12.6 \text{ tpy}
 \end{aligned}$$



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PreMod NO<sub>x</sub> = 1.24 lb/hr  
= 29.76 lb/day  
= 30 lb/day, 30 day avg

Increase = 2.88 – 1.24 lb/hr = 1.64 lb/hr  
\*24 = 39.36 lb/day increase

### **CO:**

PostMod CO (max) = (0.20 lb/mmbtu)(54.6 mmbtu/hr)  
= 10.92 lb/hr  
\*24 = 262.1 lb/day  
\*365 = 95659.2 lb/yr  
= 47.8 tpy

PreMod CO = 4.14 lb/hr  
= 99.36 lb/day  
= 101 lb/day, 30-day avg.

Increase = 10.92 – 4.14 lb/hr = 6.78 lb/hr  
\*24 = 162.72 lb/day increase

### **ROG:**

Assume 10000 ppm inlet (this value was used in Permit to Construct, 2003 test shows 10579 ppm)

PostMod R1(ROG)(max) = (10000 ppm)(2000 scfm)(16 lb/lbm)(lbm/379 cf)(1E-6)(60)  
= 50.66 lb/hr

PostMod R2(ROG)(max) = (50.66 lb/hr)(1-0.98)  
= 1.01 lb/hr  
\*24 = 24.3 lb/day  
\*365 = 8875.6 lb/yr  
= 4.4 tpy



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PreMod ROG = 0.39 lb/hr  
= 9.36 lb/day  
= 9 lb/day, 30-day avg.

Increase = 1.01 – 0.39 lb/hr = 0.62 lb/hr  
\*24 = 14.88 lb/day increase

### **SO<sub>x</sub>:**

Assume H<sub>2</sub>S = 40 ppm (P/C used 40 ppm, 2003 test showed H<sub>2</sub>S at 19.5 ppm)

PostMod SO<sub>x</sub>(max) = (40 ppm H<sub>2</sub>S)(lbmSO<sub>2</sub>/lbmH<sub>2</sub>S)(64 lbSO<sub>2</sub>/lbmSO<sub>2</sub>)(lbm/379 cf)  
\*(2000 scfm)(60)(1E-6)  
= 0.81 lb/hr  
\*24 = 19.45 lb/day  
\*365 = 7100.45 lb/yr  
= 3.6 tpy

PreMod SO<sub>x</sub> = 0.31 lb/hr  
= 7.44 lb/day  
= 8 lb/day, 30 day avg.

Increase = 0.81 – 0.31 lb/hr = 0.50 lb/hr  
\*24 = 12 lb/day increase

### **PM<sub>10</sub>:**

PM<sub>10</sub> emission factor of 17.7 lb/mmbtu is used so that emissions increase is below significance levels. 2003 test show PM<sub>10</sub> = 4 lb/mmcf

PostMod PM/PM<sub>10</sub>(max) = (17.7 lb/mmcf)(2000 scfm)(1E-6)(60)  
= 2.12 lb/hr  
\*24 = 50.98 lb/day  
\*365 = 18606.2 lb/yr  
= 9.3 tpy



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PreMod PM/PM10 = 0.91 lb/hr  
                               = 21.84 lb/day  
                               = 22 lb/day, 30 day avg.

Increase = 2.12 – 0.91 lb/hr = 1.21 lb/hr  
                               \* 24 = 29.0 lb/day increase

Emissions Summary:

	PreMod		PostMod			Increase	
	Lb/hr	Lb/day	Lb/hr	Lb/day	Lb/yr	Lb/hr	Lb/day
NOx	1.24	30	2.88	69.06	25206.2	1.64	39
CO	4.14	101	10.92	262.1	95659.2	6.78	161
ROG	0.39	9	1.01	24.3	8875.6	0.62	15
SOx	0.31	8	0.81	19.45	7100.45	0.5	11
PM10	0.91	22	2.12	50.98	18606.2	1.21	29

Modeling Analysis:

Since the heat input 54.6 mmbtu/hr is greater than 40 mmbtu/hr, Table A-1 of R1303 cannot be used.  
 SCREEN3 will be used.

Heat Input = 54.6 mmbtu/hr  
                               \*252.16 cal/btu\*hr/60 min\*min/60 sec\*1E6 = 3.82E6 cal/sec

Stack Height = (30 ft)(m/3.281 ft) = 9.14 m  
 Stack Diam. = (7 ft)(m/3.281 ft) = 2.13 m  
 Exhaust temp = 1000 degrees F = 811 R = 1084 K

NOx = 2.04 lb/hr  
                               \*464 gr/lb\*hr/60 min\*min/60 sec = 0.263 gr/sec

CO = 6.78 lb/hr  
                               \*464 gr/lb\*hr/60 min\*min/60 sec = 0.874 gr/sec



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PM = 2.8 lb/hr

\*464 gr/lb\*hr/60 min\*min/60 sec = 0.361 gr/sec

Exhaust Flow Rate Calculation:

Flare = 2000 scfm of 50% CH<sub>4</sub> and 50% CO<sub>2</sub>

At 50% CH<sub>4</sub> of 2000 scfm or 1000 SCFM of CH<sub>4</sub> (assuming 20% excess air(EA))

Products of combustion = 1000 scfm \* 13.5 (where 13.5 from Table 142 of AP40)  
= 13500 scfm

Exhaust flow rate = 13500 + 1000 (CO<sub>2</sub> Flare 3)  
= 14,500 scfm

Actual flow rate of the flue gas from the flare: Assume T outlet of flare = 1000 degrees F (811 degrees R) after atmospheric quenching.

ACFM = 14500 [(460+1000)/(460+60)]  
= 4071105 ACFM @ 1000 degree F

Modeling results show the following: (see attached SCREEN3 printouts)

	Max conc. at 118 m. (ug/m3)	Conc. at 300 m. (ug/m3)	Significant Change in AQ (ug/m3)
NOx 1-hr	4.077	2.032	20
NOx annual (*0.1)	0.4077	0.2032	1
CO 1-hr	16.89	8.415	1100
CO 8-hr (*0.8)	13.51	6.732	500
PM10 1-hr	3.015	1.502	N/A
PM10 24 hr (*0.4)	1.21	0.601	2.5
PM10 annual(*0.1)	0.302	0.150	1

The maximum NO<sub>x</sub>, CO and PM<sub>10</sub> concentrations are below the respective Significant Change in AQ concentrations.



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No modeling required for SOx and ROG

**Health Risk Assessment (Tier 2):**

See Excel Spreadsheet  
 Assume 2000 dscfm inlet flow  
 Assume 95% destruction efficiency  
 Use inlet concentrations from 2003 source test  
 Residential receptor = 300 meters (from A/N 391030)  
 Commercial receptor = 300 meters (from A/N 391030)  
 MET station = Banning

MICR residential is 0.395 in a million  
 MICR commercial is 0.0.0772 in a million

HIA and HIC are less than one.

**EVALUATION:**

Rules:

- 212: Emission increases are below threshold amounts. No public notice is required before permit issuance.
- 401: Visible emissions are not expected.
- 402: Nuisance is not expected with proper operational procedures and mitigation measures.
- 403: Fugitive emissions are not expected with water spraying.
- 431.1: H2S inlet concentration is 20 ppm (based on 2003 test), which is less than the 150 ppm allowed by this rule.  
 Emissions as H2S are:  $(20 \text{ ppm})(1025 \text{ scfm})(34 \text{ lb/lbm})(1\text{E-}6)(\text{lbm}/379 \text{ cf})(60)(24)$   
 $= 2.6 \text{ lb/day}$ , which is less than 5 lb/day.  
 Since the emissions as H2S are less than 5 lb/day, a continuous sulfur monitoring system is not required.  
 Compliance with this rule expected.
- 1150.1: This system is required per this rule. Based on the 2003 test, ROG emissions from control device is 1.84 ppm as hexane, which is less than the 20 ppm as



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hexane allowed with a 99.59% DRE, which is better than the 98% required. Even with the increase in heat input and lfg flow rate, the flare should continue to comply with 1150.1 requirements.

Reg 13: This modification has an emissions increase, so it is subject to Reg 13 requirements.  
BACT/LAER: This equipment meets the 0.06 lb/mmbtu NOx limit, 0.2 lb/mmbtu CO limit, the 0.6 second retention time and the 1400 degrees F in the stack. See flare specs in “appendix B” of A/N 391030.  
Modeling: Modeling shows that NOx, CO and PM10 increases are below Significant Change in AQ Concentration (Table A-2)

Offsets: These emissions increases qualify for Priority Reserve.

CEQA: A NOE was prepared by Riverside County was released for comment November 5, 2009. No comments were received.

1401: MICR based in Tier 2 for both residential and commercial is less than one in a million. Hazard indices are less than one.

40CFR60 Subpart WWW: Based on the 2003 and 2008 results, NMOC as hexane were measured at 1.84 ppm (99.6%) and 2.1 ppm, respectively. This is less than the allowable 20 ppm or 98% destruction efficiency. Continued compliance is expected.

40 CFR 63 Subpart AAAA: Compliance with this subpart is expected since the equipment complies with WWW.

Title V: This is a TV facility currently operating under a TV Permit issued September 9, 2008. This permit will be issued as a De Minimus Significant Revision under A/N 500900 after a 45-day EPA notice.

### **CONCLUSION:**

This project will meet all District Rules and Regulations. It is recommended that a Permit to Operate be granted subject to the attached conditions after completion of the EPA 45-day notice.